Letter to the Editor

# Improved approximate formulas for the natural frequencies of simply supported Bernoulli-Euler beams with rotational restrains at the ends 

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## 1. Introduction

An almost semi-centennial formula by Newmark and Veletsos [1] for the determination of natural frequencies of simply supported Bernoulli-Euler beams with rotational restrains at the ends has been discussed recently in Ref. [2] by Maurizi et al. Liu [3] has also established a simplified formula for restrained cantilever beams. The simplified formula is useful, for example, in assisting the structural engineers to get a quick estimation of the natural frequencies in the preliminary design stage. In Ref. [2], the maximum relative errors of the formula by Newmark and Veletsos were found to be around $2.5 \%$ for the fundamental frequency and lower for higher frequencies. In this letter, improved formulas with reduced relative errors are given.

Consider a simply supported beam with modulus of flexural rigidity $E I$, mass density per unit length $\rho A$ and span length between supports $L$. The two ends are simply supported and restrained by two rotational springs with linear stiffness $K_{r_{1}}$ and $K_{r_{2}}$. An end is hinged if $K_{r}=0$ and clamped if $K_{r} \rightarrow \infty$.

It can be shown that the exact $n$th circular natural frequency $\omega_{n}$ for the uniform BernoulliEuler beam is given by

$$
\begin{equation*}
\omega_{n}=\lambda_{n}^{2} \sqrt{\frac{E I}{\rho A L^{4}}} \tag{1}
\end{equation*}
$$

where $\lambda_{n}$ is the non-dimensional frequency parameter and is the $n$th non-zero root of the following transcendental equation (e.g. Refs. [2,4,5]):

$$
\begin{equation*}
2 R_{1} R_{2} \varphi_{1}(\lambda) \lambda^{2}+\left(R_{1}+R_{2}\right) \varphi_{6}(\lambda) \lambda-\varphi_{4}(\lambda)=0 \tag{2}
\end{equation*}
$$

[^0]with
\[

$$
\begin{gather*}
R_{1}=E I /\left(K_{r_{1}} L\right), \quad R_{2}=E I /\left(K_{r_{2}} L\right), \quad \varphi_{1}(\lambda)=\sin (\lambda) \sinh (\lambda),  \tag{3a}\\
\varphi_{4}(\lambda)=\cos (\lambda) \cosh (\lambda)-1 \quad \text { and } \quad \varphi_{6}(\lambda)=\sin (\lambda) \cosh (\lambda)-\sinh (\lambda) \cos (\lambda) . \tag{3b}
\end{gather*}
$$
\]

The determination of the roots from Eq. (2) for various values of $R_{1}$ and $R_{2}$ could be clumsy. It is desirable to have a simple but yet accurate formula for the evaluation of the natural frequencies directly.

In Ref. [1], $\lambda_{n}$ is effectively approximated by

$$
\begin{equation*}
\lambda_{n}=\pi \sqrt{\left(n+\frac{1}{2}\left(\frac{\beta_{1}}{5 n+\beta_{1}}\right)\right)\left(n+\frac{1}{2}\left(\frac{\beta_{2}}{5 n+\beta_{2}}\right)\right)} \tag{4}
\end{equation*}
$$

where $\beta_{1}=1 / R_{1}$ and $\beta_{2}=1 / R_{2}$.
Maurizi et al. [2] have verified that the above formula is accurate with around $2 \%$ in relative errors and slightly larger in absolute errors. In the following, a more accurate formula is proposed.

## 2. Simplified equation

Since the natural frequencies of the restrained beam must lie between the natural frequencies of a hinged-hinged beam (with $\lambda_{n}=n \pi$ ) and a clamped-clamped beam, it is permissible to express $\lambda_{n}$ as

$$
\begin{equation*}
\lambda_{n}=n \pi+\varepsilon_{n} \tag{5}
\end{equation*}
$$

with $\varepsilon_{n} \geqslant 0$ and $n=1,2, \ldots$
In this case, the following simplifications can be made:

$$
\begin{array}{cl}
\sin \left(\lambda_{n}\right)=(-1)^{n} \sin \left(\varepsilon_{n}\right), & \cos \left(\lambda_{n}\right)=(-1)^{n} \cos \left(\varepsilon_{n}\right) \\
\sinh \left(\lambda_{n}\right) \approx \exp \left(\lambda_{n}\right) / 2, & \cosh \left(\lambda_{n}\right) \approx \exp \left(\lambda_{n}\right) / 2 \tag{6b}
\end{array}
$$

The approximations in Eq. (6b) are very reasonable as $\exp \left(\lambda_{n}\right)$ is much bigger than $\exp \left(-\lambda_{n}\right)$. For example, when $\lambda=\pi, \exp (\lambda) / \exp (-\lambda) \approx 535$.

As a result, substituting Eq. (6) into Eq. (2), one has

$$
\begin{equation*}
(-1)^{n}\left(2 R_{1} R_{2} \sin \left(\varepsilon_{n}\right) \lambda_{n}^{2}+\left(R_{1}+R_{2}\right)\left(\sin \left(\varepsilon_{n}\right)-\cos \left(\varepsilon_{n}\right)\right) \lambda_{n}-\cos \left(\varepsilon_{n}\right)\right) \frac{\exp \left(\lambda_{n}\right)}{2}+1=0 \tag{7}
\end{equation*}
$$

Again, as $\exp \left(\lambda_{n}\right)$ should be much bigger than unity especially for large $n$, Eq. (7) could be approximated as

$$
\begin{equation*}
2 R_{1} R_{2} \sin \left(\varepsilon_{n}\right) \lambda_{n}^{2}+\left(R_{1}+R_{2}\right)\left(\sin \left(\varepsilon_{n}\right)-\cos \left(\varepsilon_{n}\right)\right) \lambda_{n}-\cos \left(\varepsilon_{n}\right)=0 \tag{8}
\end{equation*}
$$

Rearranging the terms, $\varepsilon_{n}$ can be evaluated as

$$
\begin{equation*}
\varepsilon_{n}=\tan ^{-1}\left(\frac{\left(R_{1}+R_{2}\right) \lambda_{n}+1}{2 R_{1} R_{2} \lambda_{n}^{2}+\left(R_{1}+R_{2}\right) \lambda_{n}}\right) . \tag{9}
\end{equation*}
$$

As $\lambda_{n}$ is not known initially, it can be approximated by $n \pi$ in Eq. (9). Hence, $\lambda_{n}$ in Eq. (5) could be approximated by

$$
\begin{align*}
\lambda_{n} & =n \pi+\tan ^{-1}\left(\frac{\left(R_{1}+R_{2}\right) n \pi+1}{2 R_{1} R_{2} n^{2} \pi^{2}+\left(R_{1}+R_{2}\right) n \pi}\right) \\
& =n \pi+\tan ^{-1}\left(\frac{\left(\beta_{1}+\beta_{2}\right) n \pi+\beta_{1} \beta_{2}}{2 n^{2} \pi^{2}+\left(\beta_{1}+\beta_{2}\right) n \pi}\right) . \tag{10}
\end{align*}
$$

The complexity of Eq. (10) is similar to Eq. (4). Both formulas give the exact values for simply supported beams (i.e., $\lambda_{n}=n \pi$ when $\beta_{1}=\beta_{2}=0$ ). Table 1 shows the $\lambda_{n}$ for the first five natural frequencies of various elastically restrained beam obtained by using Eq. (4) (denoted as N-V) and Eq. (10) (denoted as present). It can be seen that the present approximate formula is more accurate in general.

For the present formula, the relative errors are less than $0.1 \%$ for the third and higher natural frequencies in general. The maximum relative errors are around $0.3 \%$ when $\beta_{1}$ and $\beta_{2}$ are around 10. For the $\mathrm{N}-\mathrm{V}$ formula, the maximum errors are also around $0.3 \%$ for the third natural frequencies when the support conditions are close to a clamped-hinged beam. In fact, it has been shown [6] that $\lambda_{n}$ for the higher natural frequencies for the clamped-hinged and clamped-clamped beams can be given by $(n+1 / 4) \pi$ and $(n+1 / 2) \pi$, respectively. The present formula gives the correct values for these two limiting cases while $\mathrm{N}-\mathrm{V}$ formula only gives the correct values for the clamped-clamped conditions.

## 3. Iteration formula

For the first two natural frequencies, the relative errors are slightly higher. It can be verified that for the $\mathrm{N}-\mathrm{V}$ formula, the maximum relative error occurs when $\beta_{1}$ is large and $\beta_{2}$ is small (i.e., close to the clamped-hinged condition). The errors are around $2.5 \%$ and $0.7 \%$ for the first and second natural frequencies, respectively. For the present formula, it can be verified that the relative errors are less than $0.4 \%$ and $0.2 \%$, respectively, for the first and second natural frequencies in general. The maximum error occurs when both $\beta_{1}$ and $\beta_{2}$ are around 10 . The maximum errors are around $2.0 \%$ and $0.7 \%$ for the first and second natural frequencies, respectively.

The main source of errors in the lower frequencies is due to the approximation of $\lambda_{n}$ by $n \pi$ in Eq. (9). The accuracy can be improved if the following iterations are carried out:

$$
\begin{equation*}
\lambda_{n}^{(i+1)}=n \pi+\tan ^{-1}\left(\frac{\left(R_{1}+R_{2}\right) \lambda_{n}^{(i)}+1}{2 R_{1} R_{2}\left(\lambda_{n}^{(i)}\right)^{2}+\left(R_{1}+R_{2}\right) \lambda_{n}^{(i)}}\right), \quad i=0,1,2, \ldots \tag{11}
\end{equation*}
$$

with $\lambda_{n}^{(0)}=n \pi$. Table 2 shows the results obtained by carrying out one and two iterations. It can be seen that the results can be improved significantly by using just one iteration for $\beta_{1}=\beta_{2}=10$.

It can be verified that by carrying out one iteration, the maximum error still occurs when both $\beta_{1}$ and $\beta_{2}$ are around 10 . However, the errors are reduced to around $0.5 \%$ and $0.03 \%$ for the first and second natural frequencies, respectively. When two iterations are used, the relative error of the first and second natural frequencies can be further reduced. However, the maximum errors

Table 1
Comparison of the frequency parameters $\lambda$ between the exact values, the $\mathrm{N}-\mathrm{V}$ method and the present method

| $\beta_{1}$ | $\beta_{2}$ | Mode number |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1 | 2 | 3 | 4 | 5 |  |
| 0 | 0 | 3.141593 | 6.283185 | 9.424778 | 12.566371 | 15.707963 | Exact |
|  |  | 3.141593 | 6.283185 | 9.424778 | 12.566371 | 15.707963 | Eq. (4) (N-V) |
|  |  | 0.00\% | 0.00\% | 0.00\% | 0.00\% | 0.00\% | Error |
|  |  | 3.141593 | 6.283185 | 9.424778 | 12.566371 | 15.707963 | Eq. (10) (Present) |
|  |  | 0.00\% | 0.00\% | 0.00\% | 0.00\% | 0.00\% | Error |
| 0.01 | 10 | 3.666010 | 6.688156 | 9.752074 | 12.840018 | 15.942637 | Exact |
|  |  | 3.629408 | 6.665157 | 9.734409 | 12.825899 | 15.931101 | Eq. (4) (N-V) |
|  |  | -1.00\% | -0.34\% | -0.18\% | -0.11\% | -0.07\% | Error |
|  |  | 3.693926 | 6.701113 | 9.758974 | 12.844070 | 15.945200 | Eq. (10) (Present) |
|  |  | 0.76\% | 0.19\% | 0.07\% | 0.03\% | 0.02\% | Error |
| 10 | 10 | 4.155664 | 7.068249 | 10.065679 | 13.105264 | 16.171791 | Exact |
|  |  | 4.188790 | 7.068583 | 10.053096 | 13.089969 | 16.156762 | Eq. (4) (N-V) |
|  |  | 0.80\% | 0.00\% | -0.13\% | -0.12\% | -0.09\% | Error |
|  |  | 4.243082 | 7.117450 | 10.092109 | 13.120973 | 16.181800 | Eq. (10) (Present) |
|  |  | 2.10\% | 0.70\% | 0.26\% | 0.12\% | 0.06\% | Error |
| 0 | 100 | 3.889185 | 7.003227 | 10.118546 | 13.235413 | 16.353724 | Exact |
|  |  | 3.816990 | 6.960660 | 10.084634 | 13.204659 | 16.324194 | Eq. (4) (N-V) |
|  |  | -1.86\% | -0.61\% | -0.34\% | $-0.23 \%$ | -0.18\% | Error |
|  |  | 3.896541 | 7.009535 | 10.124258 | 13.240594 | 16.358431 | Eq. (10) (Present) |
|  |  | 0.19\% | 0.09\% | 0.06\% | 0.04\% | 0.03\% | Error |
| 1 | 10000 | 4.041438 | 7.133133 | 10.255610 | 13.386423 | 16.521079 |  |
|  |  | 4.004427 | 7.103484 | 10.231712 | $13.366776$ | 16.504431 | $\text { Eq. (4) }(N-V)$ |
|  |  | -0.92\% | -0.42\% | $-0.23 \%$ | $-0.15 \%$ | -0.10\% | Error |
|  |  | 4.063126 | 7.141534 | 10.259571 | 13.388761 | 16.522632 | Eq. (10) (Present) |
|  |  | 0.54\% | 0.12\% | 0.04\% | 0.02\% | 0.01\% | Error |
| 10000 | 10000 | 4.729095 | 7.851636 | 10.993412 | 14.134343 | 17.275311 | Exact |
|  |  | $4.711604$ | $7.852412$ | $10.993222$ | $14.134032$ | $17.274842$ | Eq. (4) (N-V) |
|  |  | $-0.37 \%$ | $0.01 \%$ | $0.00 \%$ | $0.00 \%$ | $0.00 \%$ | Error |
|  |  | 4.711761 | 7.852726 | 10.993691 | $14.134657$ | $17.275623$ | Eq. (10) (Present) |
|  |  | -0.37\% | 0.01\% | 0.00\% | 0.00\% | 0.00\% | Error |
| $\infty$ | $\infty$ | 4.730041 | 7.853205 | 10.995608 | 14.137165 | 17.278760 | Exact |
|  |  | 4.712389 | 7.853982 | 10.995574 | 14.137167 | 17.278760 | Eq. (4) (N-V) |
|  |  | $-0.37 \%$ | $0.01 \%$ | $0.00 \%$ | $0.00 \%$ | $0.00 \%$ | Error |
|  |  | $4.712389$ | $7.853982$ | $10.995574$ | $14.137167$ | $17.278760$ | Eq. (10) (Present) |
|  |  | $-0.37 \%$ | 0.01\% | $0.00 \%$ | $0.00 \%$ | $0.00 \%$ | Error |

now occur when both $\beta_{1}$ and $\beta_{2}$ are large (i.e., close to the clamped-clamped condition). The errors are around $0.4 \%$ and $0.01 \%$ for the first and second natural frequencies, respectively. This error cannot be reduced easily and is due to the assumption that $\exp \left(\lambda_{n}\right)$ is much larger than unity.

Table 2
Comparison of the frequency parameters $\lambda$ between the exact values and the present method with iterations

| $\beta_{1}$ | $\beta_{2}$ | Mode 1 |  |  |  | Mode 2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Exact solution | Iteration | Present method | Error (\%) | Exact solution | Iteration | Present method | Error (\%) |
| 0.01 | 10 | 3.666010 | 0 | 3.693926 | 0.76 | 6.688156 | 0 | 6.701113 | 0.19 |
|  |  |  | 1 | 3.664864 | $-0.03$ |  | 1 | 6.687756 | -0.01 |
|  |  |  | 2 | 3.666323 | 0.01 |  | 2 | 6.688171 | 0.00 |
| 10 | 10 | 4.155664 | 0 | 4.243082 | 2.10 | 7.068249 | 0 | 7.117450 | 0.70 |
|  |  |  | 1 | 4.133322 | $-0.54$ |  | 1 | 7.065875 | $-0.03$ |
|  |  |  | 2 | 4.143353 | $-0.30$ |  | 2 | 7.068888 | 0.01 |
| 0 | 100 | 3.889185 | 0 | 3.896541 | 0.19 | 7.003227 | 0 | 7.009535 | 0.09 |
|  |  |  | 1 | 3.889504 | 0.01 |  | 1 | 7.003173 | 0.00 |
|  |  |  | 2 | 3.889569 | 0.01 |  | 2 | 7.003228 | 0.00 |
| 1 | 10000 | 4.041438 | 0 |  | 0.54 | 7.133133 | 0 |  |  |
|  |  |  | 1 | 4.035723 | -0.14 |  | 1 | 7.133209 | $0.00$ |
|  |  |  | 2 | 4.036380 | -0.13 |  | 2 | 7.133280 | 0.00 |
| 10000 | 10000 | 4.729095 | 0 | 4.711761 | -0.37 | 7.851636 | 0 | 7.852726 | 0.01 |
|  |  |  | 1 | 4.711447 | -0.37 |  | 1 | 7.852412 | 0.01 |
|  |  |  | 2 | 4.711447 | $-0.37$ |  | 2 | 7.852412 | 0.01 |

## 4. Conclusions

In this letter, an approximate formula for the natural frequencies of simply supported Bernoulli-Euler beams with rotational restrains at the ends is given. The accuracy is better than the one given by Newmark and Veletsos in general. Compared to the exact values, the relative errors of the present formula are less than $0.3 \%$ for the third and higher natural frequencies. The relative errors of the first two natural frequencies are slightly higher and are less than $0.4 \%$ in general, except when the $\beta$ values are around 10 . When the $\beta$ values are around 10 , say $1 \leqslant \beta \leqslant 100$, it is recommended to use one or two iterations to reduce the error to $0.4 \%$.

## References

[1] N.M. Newmark, A.S. Veletsos, A simple approximation for the natural frequencies of partially restrained bars, Journal of Applied Mechanics 19 (4) (1952) 563.
[2] M.J. Maurizi, P.M. Bellés, H.D. Martín, An almost semicentennial formula for a simple approximation of the natural frequencies of Bernoulli-Euler beams, Journal of Sound and Vibration 260 (2003) 191-194.
[3] W.H. Liu, Approximate formula for determining the fundamental frequency of a restrained cantilever, Journal of Sound and Vibration 124 (1988) 204-205.
[4] M.J. Maurizi, R.E. Rossi, J.A. Reyes, Comments on a note on vibrations of generally restrained beams, Journal of Sound and Vibration 147 (1991) 167-171.
[5] T. Nànàsi, Relations between frequency equations of single-span beams, Journal of Sound and Vibration 171 (1994) 323-334.
[6] R.D. Blevins, Formulas for Natural Frequency and Mode Shape, Van Nostrand Reinhold, New York, 1979.


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